

UNCLASSIFIED COPY
DATE 10/1/84

HIGH-POWER RF COMPRESSOR

C. W. Hartman
J. H. Hammer
D. Meeker

March 30, 1984

Lawrence
Livermore
National
Laboratory

This is an informal report intended primarily for internal or limited external distribution. The opinions and conclusions stated are those of the author and may or may not be those of the Laboratory.
Work performed under the auspices of the U.S. Department of Energy by the Lawrence Livermore National Laboratory under Contract W-7405-Eng-48.

DISCLAIMER

This document was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor the University of California nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or the University of California. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or the University of California, and shall not be used for advertising or product endorsement purposes.

This report has been reproduced
directly from the best available copy.

Available to DOE and DOE contractors from the
Office of Scientific and Technical Information
P.O. Box 62, Oak Ridge, TN 37831
Prices available from (615) 576-8401, FTS 626-8401

Available to the public from the
National Technical Information Service
U.S. Department of Commerce
5285 Port Royal Rd.,
Springfield, VA 22161

HIGH-POWER RF COMPRESSOR

C. W. Hartman, J. H. Hammer, and D. Meeker
Lawrence Livermore National Laboratory, University of California
Livermore, CA 94550

I. Introduction and Summary

We discuss here the possibility of rapidly compressing resonant RF fields in a coaxial cavity with a moving, magnetically confined plasma ring. The possibility of accelerating a plasma ring and various acceleration configurations are discussed in Ref. 1. Since the ring velocity can be high, compression to high energy density and high power can be achieved before significant resistive loss or vaporization of the cavity walls occurs. An example is given of compressing 10^5 J of $\lambda = 15$ cm stored energy to 2×10^6 J of $\lambda = 1.0$ cm RF energy with the energy released in 3 nsec for a maximum power of 6×10^{14} W. A proof of principle plasma ring accelerator experiment could provide a significant test by compressing 125 joules of 14 cm RF to 1.25 kJ of 1.4 cm radiation, released in 5 nsec for a very respectable peak power of 2.5×10^{11} W.

II. RF Compressor

The compressor considered here is shown in Fig. 1. Prior to the arrival of the moving ring at $Z = L$, the region $0 < Z < L$ is filled with TE_{01} RF fields resonant with the mode $\frac{\omega_0^2}{c^2} = k_r^2 + k_z^2 \approx \left(\frac{\pi}{\Delta}\right)^2 + \left(\frac{2\pi N}{L}\right)^2$ where the number of Z wavelengths is N . ($\Delta/R \ll 1$ where R = mean radius is assumed for simplicity.) The mode chosen (see Fig. 1) has $E = E_\theta$ only, so that no electric fields terminate on conductors to avoid field emission cavity loading.

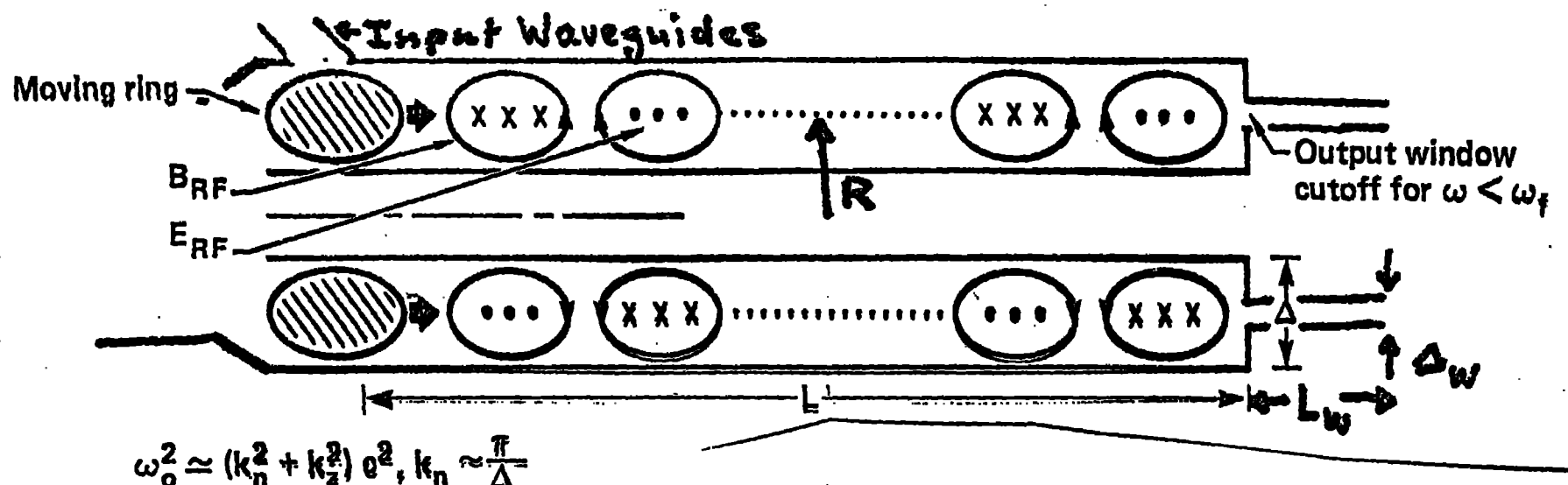
The moving ring is considered to have been accelerated by a multi-megajoule driver² to a velocity of order $V_r \approx 10^9$ cm/sec, with megagauss magnetic fields, and a plasma density of $10^{17} - 10^{18}$ cm⁻³. The ring provides a fast-moving, sliding short which compresses the cavity fields. At $Z = 0$ in Fig. 1, an output waveguide is located which has a cutoff frequency

$\frac{\omega_{co}^2}{c^2} \approx \left(\frac{\pi}{\Delta_w}\right)^2$ with $\omega_0 \ll \omega_{co}$. As the axial length of the cavity is decreased by

the moving ring, the RF resonant frequency increases as,

$\omega = c \left(\frac{\pi}{\Delta}\right) \left[1 + \left(\frac{2N\Delta}{L}\right)^2\right]^{1/2}$. The cavity energy increases until $\omega \approx \omega_{co}$ at

which time the compressed energy is released through the output waveguide.



$$\omega_o^2 \approx (k_n^2 + k_z^2) c^2, k_n \approx \frac{\pi}{\Delta}$$

$$\left. \begin{aligned} \frac{\omega}{\omega_o} &\approx \frac{L_o}{L} \\ \frac{U_{rf}}{U_{rf0}} &= \frac{L_o}{L} \end{aligned} \right\} \begin{array}{l} \text{Compression} \\ \text{laws} - \text{no} \\ \text{losses} \end{array}$$

Fig. 1. Compression of R.F. cavity modes.

To estimate the compression and release of the RF energy, we neglect losses so that the time variation of the RF energy is given by,

$$\frac{dU_{rf}}{dt} = 2\pi R \Delta \frac{B_{rf}^2}{2\mu_0} V_r - \frac{B_{rf}^2}{2\mu_0} c 2\pi R \Delta_w \exp \left\{ -2 \left[\left(\frac{\pi}{\Delta_w} \right)^2 - \frac{\omega^2}{c^2} \right]^{1/2} L_w \right\} \quad (1)$$

where the first r.h.s. term gives the increase of U_{rf} by compression and the second gives the evanescent transmission of power through the cutoff waveguide. Equation (1) can be written,

$$\dot{U}_{rf} = - U_{rf} \frac{\dot{Z}}{Z} - U_{rf} \frac{c}{Z} \frac{\Delta_w}{\Delta} \exp \left\{ -2 \left[\left(\frac{\pi}{\Delta_w} \right)^2 - \frac{\omega^2}{c^2} \right]^{1/2} L_w \right\} \quad (2)$$

where $Z = -V_r$. The second r.h.s. term is negligible until $\omega \approx \omega_{co}$ or,

$Z = Z_{co} = 2N\Delta_w$, provided $\frac{2\pi L_w}{\Delta_w} \gg 1$ as we would choose. With negligible

transmission through the output waveguide the RF energy increases as

$U_{rf} = U_0 \frac{L}{Z}$ from Eq. (2). When $\omega \approx \omega_{co}$ the second term of Eq. (2) becomes dominant.

The risetime for the transmitted power may be roughly estimated by calculating the time required for the exponent in Eq. (2) to change from 1 to 0.

For $\exp = 1$, $\left(\frac{\pi}{\Delta_w} \right)^2 - \frac{\omega^2}{c^2} = \frac{1}{4 L_w^2}$. The term $\frac{1}{4 L_w^2}$ is small, and $\omega \approx \omega_{co} = \frac{\pi c}{\Delta_w}$.

Letting $\omega = \omega_{co} - \Delta\omega$ where $\Delta\omega$ is the frequency shift for $\exp = 1$, gives

$$\Delta\omega = \frac{c^2}{8 L_w^2 \omega_{co}}. \text{ Setting } \Delta\omega = \dot{\omega} \tau_{rise} \text{ where, } \dot{\omega} \approx \omega_{co} \frac{V_r}{Z_{co}} \text{ gives } \tau_{rise} = \frac{c^2 Z_{co}}{8 L_w^2 \omega_{co}^2 V_r}$$

$$= \frac{N \Delta_w^3}{4\pi^2 L_w^2 V_r}. \text{ If } \tau_{rise} \text{ is shorter than the light transit time for the cutoff}$$

waveguide, L_w/c , then $\tau_{rise} = L_w/c$ should be used. Once the cutoff frequency is exceeded, the RF power transmitted through the guide exceeds the compression

term by $c\Delta_w/V_r\Delta > 1$. The RF field then decays from Eq. (2) as,

$$\dot{U}_{rf} \approx - U_{rf} \frac{c}{Z_{co}} \frac{\Delta_w}{\Delta} \quad (3)$$

i.e., with a time constant $\tau_{decay} \approx \frac{Z_{co}}{c} \frac{\Delta}{\Delta_w}$. The maximum stored U_{rf} is

$U_{max} = U_o \frac{L}{Z_{co}}$ and the maximum power is, $P_{max} = \frac{U_o L}{Z_{co}} \frac{c}{Z_{co}} \left(\frac{\Delta_w}{\Delta}\right)$. The output is shown in Fig. 2.

As an example, we consider an initial cavity length $L = 100$ cm with

$\Delta = 10$ cm, and $N = \frac{L}{2\Delta} = 5$ wavelengths in the z-direction. The initial resonant

frequency is $f = 2000$ Hz ($\lambda_o = 15$ cm). Prior to the ring's arrival, a 2 μ sec pulse of 50 GW power is used to establish 100 kJ of stored RF energy in the cavity. The ring compresses the RF field energy 20-fold at 10^9 cm/sec until $\lambda = \lambda_{co}$ (taken here to be $\lambda_{co} = 1.0$ cm). At $Z = Z_{co} = 5$ cm, U_{rf} has increased to 2 MJ and the output waveguide begins to transmit. The power rises

in $\tau_{rise} = \frac{L_w}{c} \approx .15$ nsec to $P_{max} = 6 \times 10^{14}$ watts and decays with a time constant $\tau_{decay} = 3$ nsec.

Appendix A discusses a similar example of RF compression by a lower energy ring as might be produced in a proof of principle experiment.

III. Loss

Next, consider losses, first in the cavity walls and then in the ring.

Since, the electrical skin depth $\delta = \sqrt{\frac{\eta}{\omega\mu_o}}$ is less than the thermal skin

depth, $\delta_{th} = \sqrt{\frac{\kappa}{C\tau}}$ for $\omega\tau \gg 1$, the surface temperature of the cavity walls during filling is,

$$T_s = \frac{4}{3\sqrt{\pi}} \frac{P_o}{t_o} \frac{t^{3/2}}{\sqrt{C\kappa}} \quad (4)$$

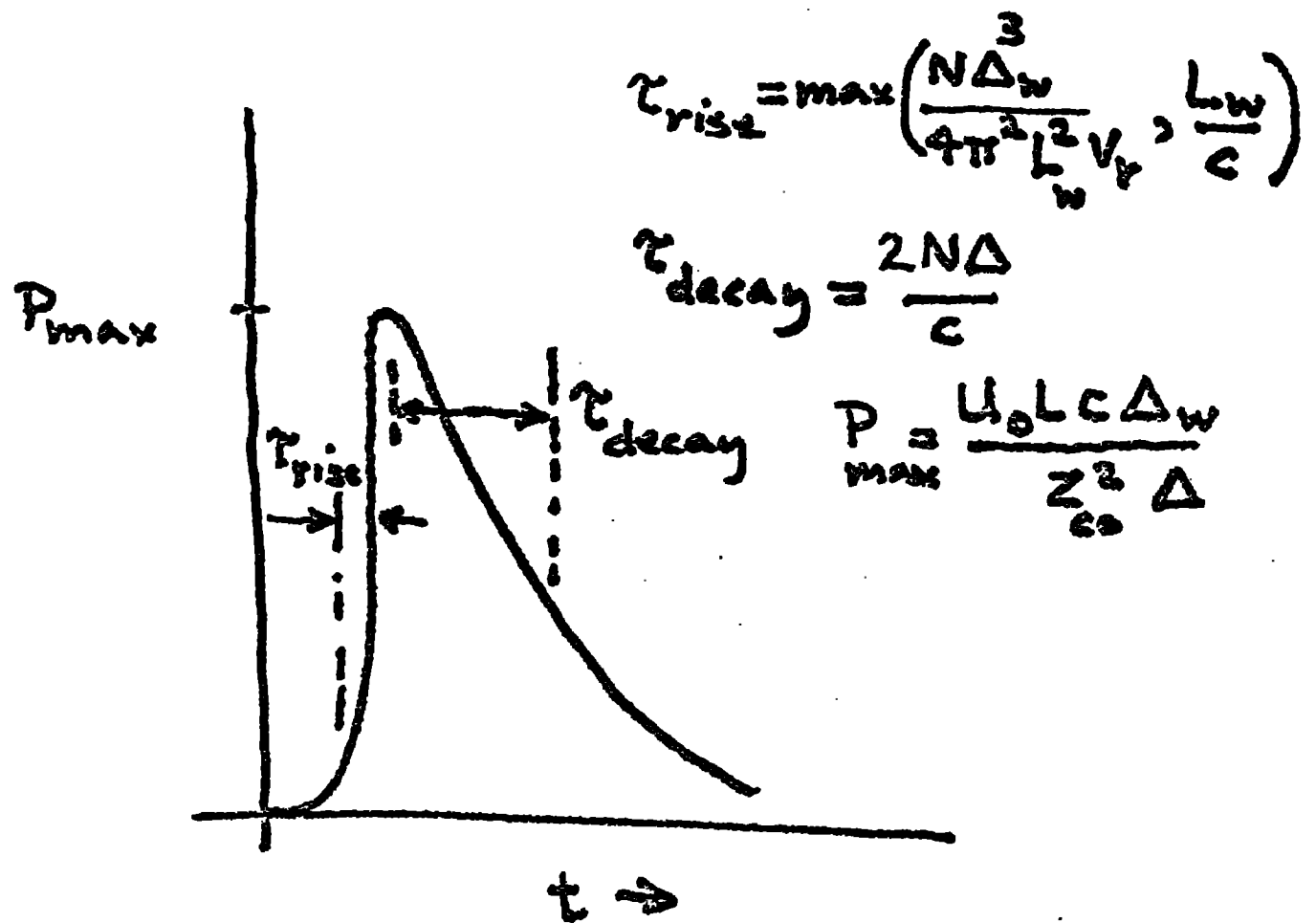


Figure 2. P_{rf} vs time.

where the power incident on the walls is $P_{\text{walls}} \approx \omega \frac{B_{\text{rf}}^2}{2\mu_0} \delta = P_0 \frac{t}{t_0}$ watts/cm²

(a linear time dependence of the incident power is used for simplicity).

For the example considered in Section II (100 kJ RF at $\lambda = 15$ cm, $L = 100$ cm, $\Delta = 10$ cm and $R = 10$ cm, $B_{\text{rf max}} \approx 20$ kG), $\delta = 10^{-4}$ cm, and $P_0 = 2 \times 10^4$ w/cm². Setting $t = t_0$ in Eq. (4) gives a temperature rise $T_s \approx 1000^\circ\text{C}$.

During compression by the ring, $U_{\text{rf}} \propto Z^{-1}$ and $\omega \propto \frac{1}{Z}$ giving $P_{\text{walls}} \propto$

$B_{\text{rf}}^2 \delta \omega \sim \frac{U_{\text{rf}}}{Z} \omega^{1/2} \sim \frac{1}{Z^{5/2}}$ so that the wall power rises very rapidly as $Z \rightarrow Z_{\text{co}}$.

At $Z = Z_{\text{co}} = 5$ cm, $U_{\text{rf max}} = 2 \times 10^6$ j, $B_{\text{rf}} = 400$ kG, and $P_0 = 3 \times 10^9$ w/cm².

Taking the characteristic time for power rise t_0 to be $\frac{Z_{\text{co}}}{V_r} \approx 5$ nsec, the energy

investment in the wall surface from Eq. (4) is $CT_s = 2. \times 10^5$ j/cm³.

This energy density corresponds to about 3 eV per atom, i.e., sufficient for vaporization of the surface. The total energy lost in the walls is about 40 kJ or 2% of the RF energy. Additional losses due to vaporization may occur, however, it is useful to observe that at 1 eV a copper atom can move only 10^{-3} cm in the final 5 nsec of compression.

RF losses in the ring are too difficult to evaluate in detail in this preliminary note. We observe that the induced currents are azimuthal so that electrode sheaths should not be important. In order to compress to $B_{\text{rf}} \approx 400$ kG, it appears likely that the ring field should be about as large as B_{rf} . Taking $B_{\text{ring}} = 500$ kG as an example, the electron/ion cyclotron frequencies are $f_{\text{ce}}/f_{\text{ci}} = 1.5 \times 10^{12}/4 \times 10^8$ Hz for hydrogen while the RF frequency ranges from $.2 - 3 \times 10^{10}$ Hz. Gyroresonances in the main ring region are therefore not expected. The plasma density of the ring might be $n_e \approx 10^{17}$ cm⁻³ which is well beyond cutoff, even at the highest RF frequency ($n_{\text{comax}} \approx 10^{13}$ cm⁻³).

In the absence of turbulence the RF current tends to flow in a small thickness skin. At $n_e = 10^{17}$ cm⁻³, the collision-free skin depth is small, $\delta_{\text{cf}} \approx 2 \times 10^{-3}$ cm, and at surface currents $I' \approx .4$ MA/cm the drift speed required $v_D = \frac{I'}{n_e \delta_{\text{cf}} e}$ is $v_D \approx 10^{10}$ cm/sec ($E = 30$ keV drift energy). Instabilities will tend to heat and broaden the layer. Taking a

broadened skin depth $\delta \approx 10 \delta_{cf} \approx 2 \times 10^{-2}$ cm, gives $E_D \approx 300$ eV. Even if the full RF energy is deposited in width δ each radian the total losses during the

final compression time $\tau = 5$ ns would be roughly $\frac{B_{rf}^2}{2 \mu_0} \tau \omega \delta 2\pi R \Delta \approx 10^5$ joules

or 5% of U_{rf} max.

APPENDIX A. PROOF OF PRINCIPLE RF COMPRESSOR

We have considered a high-energy RF compressor which would use a corresponding high energy ring such as might be obtained using the Shiva-Star 9.3 MJ bank. Here we consider an RF compression test using a moving ring having parameters approximating those which might be achieved in the proof of principle experiment.

Under typical conditions we would expect to produce in the POP experiment a ring having the parameters shown in Fig. 3.

As in the high energy case, we consider a coaxial cavity (Fig. 1) 100 cm long prefilled with 125 J of a $\lambda_0 = 14$ cm cavity mode having $N = 7$ wavelengths in the z direction. The output waveguide has a cutoff wavelength $\lambda_f = 1.4$ cm corresponding to a 10-fold compression of the RF energy to 1.25 KJ before transmission. At final compression ($L_f = 10$ cm) the RF field has increased to $B_{rf} = 5$ kG, or roughly 1/2 of the ring field.

When $\omega_{rf} > \omega_{co}$ ($\lambda_f \approx 1.4$ cm) the transmitted power increases to

$$P_{\max} \approx U_{rf} \max \frac{\Delta_w}{\Delta} \frac{c}{L_f} \approx 250 \text{ G watt and decays with a time constant } \tau = 5 \text{ nsec.}$$

The temperature rise of the RF cavity walls is predicted to be modest ($< 100^\circ\text{C}$) for this case. A test at this, not insignificant, power level would provide information on RF losses in the ring at $B_{rf} \approx 1/2 B_{\text{ring}}$.

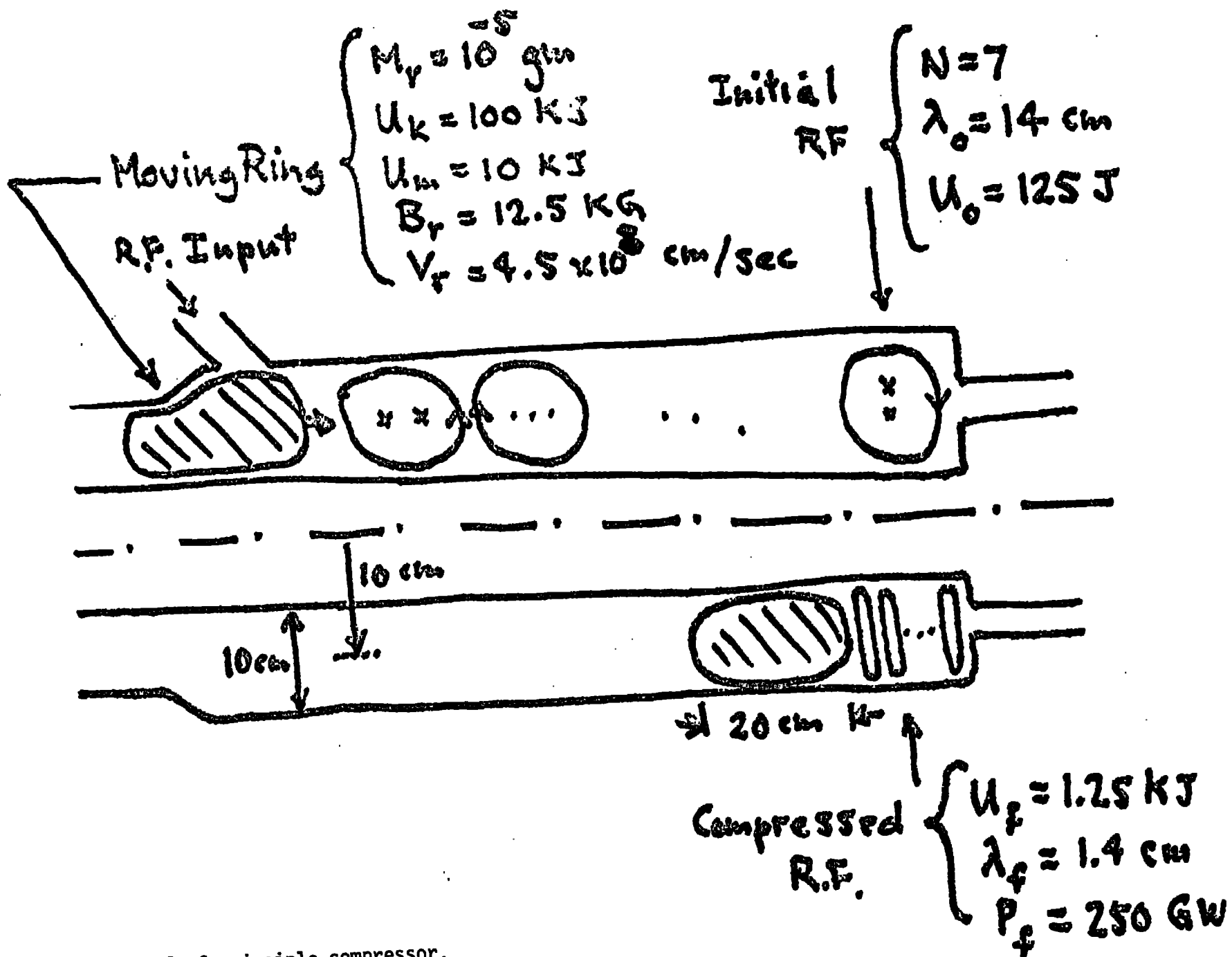


Fig. 3. Proof of principle compressor.

REFERENCES

1. C. W. Hartman and J. H. Hammer, Phys. Rev. Lett. 48 (1982) 929.
2. C. W. Hartman et al., Proceedings of the Fifth Symposium on The Physics and Technology of Compact Toroids, Nov. 16-18, 1982.